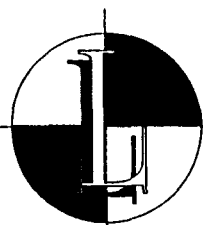


GAËTAN H. LASCELLES ING.
P. ENG.
MANON C. RODRIGUE ING.
P. ENG.



L04-120
March 11, 2005

South Nation Conservation
15 Union Street
Berwick, Ontario K0C 1G0

By Fax: (613) 984-2872
Attention: Sandra Mancini

Dear Ms. Mancini:

Re: Stormwater Management Study
Robert Lafrance Subdivision, St-Eugène
Part of Lot 13, Concession 4, Township of East Hawkesbury

Enclosed please find the site grading and drainage plan and the Stormwater Management Study for the Robert Lafrance Subdivision located on Part of Lot 13, concession 4 in the Township of East Hawkesbury.

The Stormwater Management Study shows that the proposed development of the site with grassed swale results in post-development flows increase of up to 4.8 L/sec for the time of concentration of 20 minutes or an equivalent of 5700 litres for storms up to the 100-year event. The additional flow of 4.8 L/sec (0.0048 m³/sec) for the 100 year storm is equivalent to 0.8% of the flow measured on that day in the creek which can accommodate the minimal additional flow. It is recommended that the proposed development be carried out in accordance with the site grading plan with proposed drainage directed away from buildings and towards swale at the rear of the lots and the existing ditches along County Road 14 with the use of sediment and erosion control measures in accordance with best management practices as listed above.

We trust the enclosed is to your satisfaction and we remain,

Yours truly,
L'ingénierie
LASCELLES
engineering limited

per: Manon C. Rodrigue
Manon C. Rodrigue, P.Eng.

encl.

cc: Robert Lafrance
Louis Prévost, UCPR

Stormwater Management Study.

The site is located on the west side of County Road 14 in St-Eugene. County Road 14 is a paved road with gravel shoulders and drainage ditches. There is a 0.46 C.S.P. culvert at entrance to lot 6. The site is located on part of lot 13, Concession 4 in the township of East Hawkesbury, being part 3 of plan 46R-5423. The house at the site is located at civic number 4700 County Road no.14 and the total site frontage is 361.79 m and the depth is 76.215 m a total area of 2.75 ha. The site is relatively flat. The proposed lots 1 to 4 have areas of 4594 m² while lot 5 has an area of 4595 m² and the retained lot 6 has an area of 4538 m². Drainage is overland towards a ditch along County Road 14. There is a house with detached garage located on lot 6, civic number 4700 and gravel driveway. Surrounding land use are residential and agricultural. The site is located across from a strip development. According to the test pits dug on site and to the soil map of Prescott County the soil at the site is a sandy loam over clay described as Uplands fine sandy loam described as reddish brown, loose sandy soils with sorted non-calcareous fine sand parent material with a hydrologic soil group A.

The stormwater management study was prepared using the Rational Method for a 5-year and 10-year storm with the following runoff coefficients for the site.

Rational Method:

$$Q = 2.78 \text{ CIA}$$

Runoff Coefficients: (C)

Roof	0.9
Gravel	0.5
Pasture	0.15
Lawns	0.10

For a 25-year return storm, the runoff coefficients are increased by 10%.

For a 50-year return storm, the runoff coefficients are increased by 20%

For a 100-year return storm, the runoff coefficients are increased by 25%

The time of concentration was calculated using the Airport formula for a drainage coefficient of less than 0.4. The airport formula is:

$$T_c = \frac{3.26 (1.1 - C) L^{0.5}}{S^{0.33}}$$

$$\text{and } S = \frac{100 (\Delta h - h_f)}{0.75 L - L_f} \%$$

$$\text{Thus } S = \frac{100 (58.4 - 56.3)}{0.75 \times 200} = 1.4 \%$$

and

$$T = \frac{3.26 (1.1 - 0.15) 200^{0.5}}{1.4^{0.33}} = 18.33 \text{ minutes, Say 20 minutes}$$

The rainstorm intensity was obtained from an intensity-duration-frequency table for the Ottawa Airport. The following intensity were used for the study for a time of concentration of 20 minutes.

5-year return period storm: rainfall intensity is 68.0 mm/hr
10-year return period storm: rainfall intensity is 79.0 mm/hr
25-year return period storm: rainfall intensity is 92.1 mm/hr
50-year return period storm: rainfall intensity is 101.8 mm/hr
100-year return period storm: rainfall intensity is 111.6 mm/hr

The area for the pre-development is the totality of the site which drained towards the front yard ditch and towards the rear of the site.

Pre-development Runoff:

The pre-development runoff is directed towards the ditch at the street (Area 1), towards the ditch offsite at the rear (Area 2 and 3).

$$\text{Area 1 coefficient } C = (0.025 \times 0.5 + 0.2008 \times 0.10 + 0.4265 \times 0.15) / 0.6523 = 0.148$$

Area 1:

Flow	Volume
Q pre 5-year = $2.78 \times 68 \times 0.148 \times 0.6523 = 18.2 \text{ L/sec}$	$18.2 \text{ L/sec} \times 20 \text{ min} = 21.8 \text{ m}^3$
Q pre 10-year = $2.78 \times 79 \times 0.148 \times 0.6523 = 21.2 \text{ L/sec}$	$21.2 \text{ L/sec} \times 20 \text{ min} = 25.4 \text{ m}^3$
Q pre 25-year = $2.78 \times 92.1 \times 0.148 \times 1.1 \times 0.6523 = 27.2 \text{ L/sec}$	$27.2 \text{ L/sec} \times 20 \text{ min} = 32.6 \text{ m}^3$
Q pre 50-year = $2.78 \times 101.8 \times 0.148 \times 1.2 \times 0.6523 = 32.8 \text{ L/sec}$	$32.8 \text{ L/sec} \times 20 \text{ min} = 39.4 \text{ m}^3$
Q pre 100-year = $2.78 \times 111.6 \times 0.148 \times 1.25 \times 0.6523 = 37.4 \text{ L/sec}$	$37.4 \text{ L/sec} \times 20 \text{ min} = 44.9 \text{ m}^3$

$$\text{Area 2 \& 3 coefficient } C = (0.0240 \times 0.9 + 0.2040 \times 0.1 + 1.8706 \times 0.15) / 2.0986 = 0.154$$

Area 2 & 3:

Flow	Volume
Q pre 5-year = $2.78 \times 68 \times 0.154 \times 2.0986 = 61.1 \text{ L/sec}$	$61.1 \text{ L/sec} \times 20 \text{ min} = 73.3 \text{ m}^3$
Q pre 10-year = $2.78 \times 79 \times 0.154 \times 2.0986 = 71.0 \text{ L/sec}$	$71.0 \text{ L/sec} \times 20 \text{ min} = 85.2 \text{ m}^3$
Q pre 25-year = $2.78 \times 92.1 \times 0.154 \times 1.1 \times 2.0986 = 91.0 \text{ L/sec}$	$91.0 \text{ L/sec} \times 20 \text{ min} = 109.2 \text{ m}^3$
Q pre 50-year = $2.78 \times 101.8 \times 0.154 \times 1.2 \times 2.0986 = 109.8 \text{ L/sec}$	$109.8 \text{ L/sec} \times 20 \text{ min} = 131.8 \text{ m}^3$
Q pre 100-year = $2.78 \times 111.6 \times 0.154 \times 1.25 \times 2.0986 = 125.3 \text{ L/sec}$	$125.3 \text{ L/sec} \times 20 \text{ min} = 150.4 \text{ m}^3$

Total offsite is as follows

Q pre 5-year = $18.2 \text{ L/sec} + 61.1 \text{ L/sec} = 79.3 \text{ Lsec}$	$21.8 \text{ m}^3 + 73.3 \text{ m}^3 = 95.1 \text{ m}^3$
Q pre 10-year = $21.2 \text{ L/sec} + 71.0 \text{ L/sec} = 92.2 \text{ Lsec}$	$25.4 \text{ m}^3 + 85.2 \text{ m}^3 = 110.6 \text{ m}^3$
Q pre 25-year = $27.2 \text{ L/sec} + 91.0 \text{ L/sec} = 118.2 \text{ Lsec}$	$32.6 \text{ m}^3 + 109.2 \text{ m}^3 = 141.8 \text{ m}^3$
Q pre 50-year = $32.8 \text{ L/sec} + 109.8 \text{ L/sec} = 142.6 \text{ Lsec}$	$39.4 \text{ m}^3 + 131.8 \text{ m}^3 = 171.2 \text{ m}^3$
Q pre 100-year = $37.4 \text{ L/sec} + 125.3 \text{ L/sec} = 162.7 \text{ Lsec}$	$44.9 \text{ m}^3 + 150.4 \text{ m}^3 = 195.3 \text{ m}^3$

The proposed site conditions are as follows:

With proposed development and grading and drainage with ditch at back of lots the time of concentration for the developed conditions becomes:

$$S = \frac{100(57.2 - 55.6)}{0.75 \times 150} = 1.4 \%$$

and

$$T = \frac{3.26(1.1 - 0.15) 200^{0.5}}{1.4^{0.33}} = 18.33 \text{ minutes, Say 20 minutes}$$

Total of five new developed suburban residential site and one existing residential lot.

Roof Area = 0.0240 ha per lot

Grass Area = 0.4194 ha per lot, lot 5 has 0.4195 ha, lot 6 has 0.4048 ha

Gravel Area = 0.0160 ha per lot, lot 6 has 0.025 ha

$$\text{Therefore equivalent } C = \frac{(6 \times 0.0240 \times 0.9 + (4 \times 0.4194 + 0.4195 + 0.4048) \times 0.1 + (5 \times 0.016 + 0.025) \times 0.5)}{2.7509} = 0.157$$

Flow

$$Q \text{ post 5-year} = 2.78 \times 68 \times 0.157 \times 2.7509 = 81.6 \text{ L/sec}$$

$$Q \text{ post 10-year} = 2.78 \times 79 \times 0.157 \times 2.7509 = 94.9 \text{ L/sec}$$

$$Q \text{ post 25-year} = 2.78 \times 92.1 \times 0.157 \times 1.1 \times 2.7509 = 121.6 \text{ L/sec}$$

$$Q \text{ post 50-year} = 2.78 \times 101.8 \times 0.157 \times 1.2 \times 2.7509 = 146.7 \text{ L/sec}$$

$$Q \text{ post 100-year} = 2.78 \times 111.6 \times 0.157 \times 1.25 \times 2.7509 = 167.5 \text{ L/sec}$$

Volume

$$81.6 \text{ L/sec} \times 20 \text{ min} = 97.9 \text{ m}^3$$

$$94.9 \text{ L/sec} \times 20 \text{ min} = 113.9 \text{ m}^3$$

$$121.6 \text{ L/sec} \times 20 \text{ min} = 145.9 \text{ m}^3$$

$$146.7 \text{ L/sec} \times 20 \text{ min} = 176.0 \text{ m}^3$$

$$167.5 \text{ L/sec} \times 20 \text{ min} = 201.0 \text{ m}^3$$

Therefore the difference between the pre and post development for the different return period are as follows:

Flow

$$5\text{-year} = 81.6 \text{ L/sec} - 79.3 \text{ L/sec} = 2.3 \text{ L/sec}$$

$$10\text{-year} = 94.9 \text{ L/sec} - 92.2 \text{ L/sec} = 2.7 \text{ L/sec}$$

$$25\text{-year} = 121.6 \text{ L/sec} - 118.2 \text{ L/sec} = 3.4 \text{ L/sec}$$

$$50\text{-year} = 146.7 \text{ L/sec} - 142.6 \text{ L/sec} = 4.1 \text{ L/sec}$$

$$100\text{-year} = 167.5 \text{ L/sec} - 162.7 \text{ L/sec} = 4.8 \text{ L/sec}$$

Volume

$$97.9 \text{ m}^3 - 95.1 \text{ m}^3 = 2.8 \text{ m}^3$$

$$113.9 \text{ m}^3 - 110.6 \text{ m}^3 = 3.3 \text{ m}^3$$

$$145.9 \text{ m}^3 - 141.8 \text{ m}^3 = 4.1 \text{ m}^3$$

$$176.0 \text{ m}^3 - 171.2 \text{ m}^3 = 4.8 \text{ m}^3$$

$$201.0 \text{ m}^3 - 195.3 \text{ m}^3 = 5.7 \text{ m}^3$$

The proposed lot grading with shallow ditch at the rear and drainage directed away from house and towards the rear and front of the house results in a volume of 5700 litres above the pre-development runoff volumes for the 100 year storm. This increase in volume is directed towards the creek at the north of the site. The creek crosses county road 14 through a 16 feet wide concrete box culvert. At the time of soil testing the flow rate was calculated at 0.6 m³/sec at the culvert. The additional flow of 4.8 L/sec (0.0048 m³/sec) for the 100 year storm is equivalent to 0.8% of the flow measured on that day. The creek can accommodate the additional flow.

Sediment and Erosion Control Measures

The following best management practices shall be implemented at various stages of construction.

Prior to construction

1) Install sediment retention control measures such as silt fence and / or straw bales between the work areas and any drainage ditch or surface water drainage areas. Perform regular maintenance of drainage ditches during construction.

During construction

- 1) Equipment maintenance shall be performed at the entrance to the site. No refuelling to take place within 5 metres from a watercourse or drainage ditch. Equipment cannot be cleaned in the watercourse. Excess fuels, lubricants, pesticides and other supplies to be removed from the site and disposed of in an approved manner.
- 2) Minimise the spread of the work area and the duration of the construction.
- 3) Surplus material must adequately be deposited at pre-approved sites.
- 4) Perform regular maintenance of drainage ditches during construction.
- 5) Upon completion of work, all accumulated sediment, debris and work related material shall be removed and properly disposed of.
- 6) Site grading for each lot to be sloped in order to shed water away from the foundation.

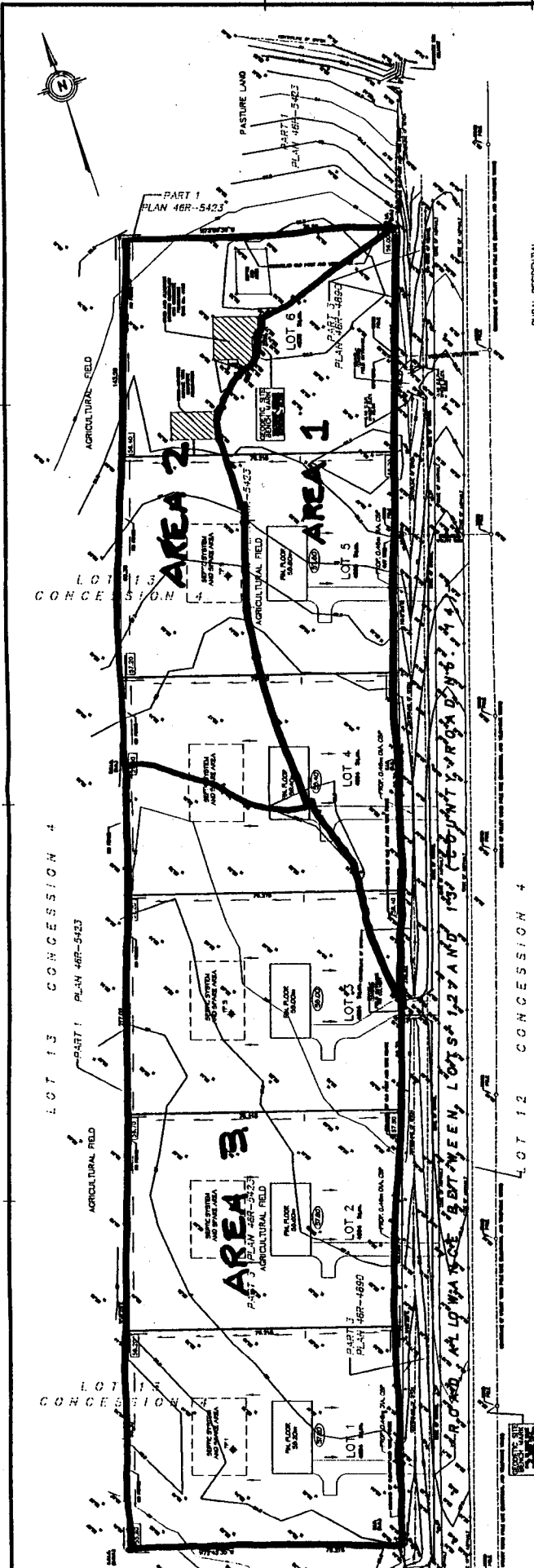
It is recommended that the proposed development be carried out in accordance with the site grading plan with proposed drainage directed away from buildings and towards swale at the rear of the lots and the existing ditches along County Road 14 with the use of sediment and erosion control measures in accordance with best management practices as listed above. We trust the above is to your satisfaction and we remain,

Yours truly,

L'ingénierie
LASCELLES
engineering limited

per: M. Rodrigue
Manon C. Rodrigue, P.Eng.





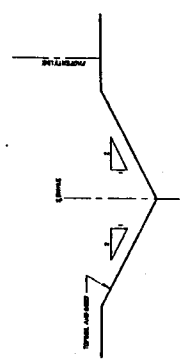
PLAN 1:500

LEGEND

- EXISTING ROAD
- PROPOSED ENTRANCE
- EDGE OF GRAVEL
- PROPOSED DRAINAGE ELEVATION
- PROPOSED DRAINAGE FLOW PATH
- PROPOSED GROUND ELEV. AROUND BLOS
- SURFACE WATER RUN-OFF

NOTES

1. EROSION AND SEDIMENT CONTROL MEASURES.
 - PRIOR TO THE START OF CONSTRUCTION, PRIOR TO THE REMOVAL OF ANY EXISTING COVER, WORKING OF SOIL, AND CONSTRUCTION, INSTALL STAKED HAY BALE FENCE OR SILT FENCE ALONG DITCHES IMMEDIATELY DOWNSTREAM FROM AREAS TO BE DISTURBED.
 - INSPECT MEASURES IMMEDIATELY AFTER INSTALLATION.
2. DURING CONSTRUCTION.
 - MAINTAIN THE EXTENT OF DISTURBED AREAS AND THE DURATION OF EXPOSURE.
 - PROTECT DISTURBED AREAS FROM RAINFALL.
 - PRIOR TO THE START OF CONSTRUCTION, PRIOR TO THE REMOVAL OF ANY EXISTING COVER, WORKING OF SOIL, AND CONSTRUCTION, IF DISTURBED AREAS WILL NOT BE REVEGETATED IMMEDIATELY, INSTALL STAKED HAY BALE FENCE, SILT FENCES REGULARLY AND AFTER EVERY MAJOR STORM EVENT AND CLEAN AND REPAIR WHEN NECESSARY.
 - CONSTRUCT DRAINAGE AND SUBDRAINAGE DETAILS ON THIS PLAN.
3. AFTER CONSTRUCTION.
 - PROVIDE PERMANENT COVER CONSISTING OF TURF, SOIL AND SEED TO DISTURBED AREAS.
 - REMOVE ALL EXISTING HAY BALE FENCE, SILT FENCES AFTER DISTURBED AREAS HAVE BEEN REVEGETATED AND STABILIZED.



DATE	10/10/2003
BY	ROBERT LAFRANCE
CHECKED BY	ROBERT LAFRANCE
APPROVED BY	ROBERT LAFRANCE
PROJECT NO.	1807
SHEET NO.	104-120
PROJECT NAME	LOT GRADING PLAN
PROPOSED SUBDIVISION	COUNTY ROAD 104
ST-EUGENE, ONTARIO	
DATE	MARCH 2003
BY	GEL
CHECKED BY	M.C.S.
APPROVED BY	M.C.S.

DRAINAGE AREAS PRE-DEVELOPMENT

Prescott Russell

Canton de Township of
EAST HAWKESBURY EST



Kilomètres - Kilometres

1:80 000



